S/169/62/000/004/095/103
D230/D307

Electrophotometric measurements of ...

year showed that I_{5300} was relatively low and fairly constant. I_{6050} was also fairly constant; its variations were similar to those of I_{5300}. I_{5577} varied irregularly with a small maximum in the autumn; it was considerably larger than the other intensities. I_{5893} varied smoothly during the year with a maximum in the autumn and winter, and a minimum in the summer. I_{6300} does not have a characteristic yearly variation, but all stations recorded a small maximum in the autumn. I_{OH} showed a small maximum in the winter. The observations were divided into five groups on the basis of five very different types of nocturnal variation; the number of observations with a given type of nocturnal variation was expressed as a percentage of the total number of observations. I_{5300} and I_{6050} do not change during the night in 50 - 80 % of the observations. I_{5577} shows a nocturnal maximum in 40 %, and a minimum in 10 % of the observations. I_{6300} has a nocturnal minimum in 50 - 70 % of the

Card 3/4

S/169/62/[illegible]
D230/D302

Electrophotometric measurements of ...

observations, and some variation occurs in a small [illegible]. I_{5893} is mostly steady, while I_{OH} shows a maximum in [illegible] 6- [illegible]. The intensities at different wavelengths at all three stations were compared throughout the IGY. No correlation was found between I_{5300} and I_{5577}, I_{5577} and I_{5890}, I_{5890} and I_{6300}, I_{6050} and I_{6300}, or I_{6300} and I_{OH}. A strong correlation was found between I_{5300} and I_{6050}, and I_{5890} and I_{6050}. [Abstracter's note: Complete translation].

Card 4/4

S/030/61/000/009/004/[illegible]
B10[illegible]/B206

AUTHOR: Mironov, A. V., Candidate of Physical and Mathematical Sciences

TITLE: Investigation of the radiation of the night sky and aurorae polares

PERIODICAL: Akademiya nauk SSSR. Vestnik, no. 9, 1961, 118-119

TEXT: An Interdepartmental Conference on the Investigation of the Auroras Polaris and the Radiation of the Night Sky was held at the Institut fiziki atmosfery Akademii nauk SSSR (Institute of Physics of the Atmosphere of the Academy of Sciences USSR) from April 25 to 27, 1961. The results of spectral and electrophotometric observations of aurorae polares and the night sky made in the USSR during the last few years according to the program of the International Geophysical Year, were discussed. The following reports are mentioned: A. I. Lebedinskiy reported that much material was obtained at a number of northern stations by means of wide-angle cameras; L. S. Yevlashin reported on results of investigating the spectra of high-latitude aurorae polares by means of a wide-angle spectral

Card 1/3

S/[illegible]/61/000/006/004/00[illegible]
B10[illegible]/B206

Investigation of the radiation of...

camera at the Polyarnyy geofizicheskiy institut (Polar Geophysical Institute); V. I. Krasovskiy discussed the material from the Institute of Physics of the Atmosphere of the Academy of Sciences USSR on spectral and electrophotometric observations of aurorae polares and the radiation of the night sky. During the International Geophysical Year observations were made at three stations: Loparskaya (near Murmansk), Roshchino (near Leningrad), and Zvenigorod (near Moscow). Yu. I. Gal'perin reported on the hydrogen radiation in the aurorae polares, the velocity of motion of the hydrogen atoms relatively to the earth being calculated at 300-400 km/sec; O. L. Vaysberg reported on spectrophotometric measurements of emissions from aurorae polares by the Loparskaya station; T. M. Mulyarchik established that the temperature corresponding to the red oxygen line during high aurorae polares increases from 1000 to 3000°K, and the temperature of the green oxygen line for various low aurorae polares fluctuates between 150 and 350°K; N. V. Dzhordzhio reported on electrophotometric observations, the rules of the pulsating of aurorae polares being established; N. N. Shefov reported on the helium radiation in aurorae polares which were first recorded at the Zvenigorod station from February 10 to 11, 1958; N. I. Fedorova proved the assumption that helium emission

Card 2/3

S/030/61/000/006/004/00
B105/B206

Investigation of the radiation of...

develops in aurorae polares when they are irradiated by the sun; P V Shcheglov observed helium emission during twilight by an interferometric method; V I Ivanchuk reported on the classification of aurorae polares; S K Vsekhsvyatskiy pointed out the doublet structure of the radiation of northern light; S P Samsonov, I. S. Zaretskiy, and A V. Buk discussed the azimuthal distribution of rays and beams according to observations by the Yakutsk network of stations; Ye. A Ponomarev reported on the correlation between marine currents and aurorae polares; Ya. I. Fel'dshteyn, E K Solomatina, and G A. Rubo reported on the geographical distribution of the aurora polaris and its correlation with magnetic ionospheric fluctuations; V I Cherdnichenko discussed the corpuscular mechanism of excitation of the ultraviolet emission in low-latitude aurorae; Yu. I Gal'perin and I A Lavrova reported on relative occupation densities of the levels of atomic oxygen on the basis of spectra of aurorae polares at the Loparskaya and Zvenigorod stations; V. I. Krasovskiy established that the direct determination of the hydrogen content in the upper atmosphere, conducted in the USA, necessitates checking of the hypothesis on the nature of hydroxyl radiations

Card 4/

13438

S/169/62/000/011/067/077
D228/D307

AUTHOR: Mironov, A.V.

TITLE: Descriptions of auroras according to observations at Stn. Zvenigorod

PERIODICAL: Referativnyy zhurnal, Geofizika, no. 11, 1962, 22, abstract 11G146 (In collection: Polyarn. siyaniya i svecheniye nochn. neba, no. 8, M., AN SSSR, 1962, 24-31 (summary in Eng.))

TEXT: Spectrographic auroral observations that were carried out at Stn. Zvenigorod from 1956 are described. Auroras were observed mostly as diffuse spots, homogeneous arcs, and arcs with a radiant structure. Sometimes they appeared as vertical columns. The observations of auroras were accompanied by the registration of the magnetic activity. The emissions OI λλ 5577, 6300, and 6364 Å occur without fail in the spectra recorded at night with the auroras. In addition there are also often Na and OH emissions in the spectra. A system of N_2^+ bands and the atomic nitrogen line [NI] λ 5200 Å

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S/169/62/000/011/067/077
D228/D307

Descriptions of auroras ...

were noted in all, relatively strong auroras. The emission NII and OI ($\lambda\lambda$ 6158, 6456 Å) was observed much more rarely. Hydrogen emission (λ 6562 Å) was recorded in some cases. Helium emission (λ 10830 Å) was detected on the occasion of one intense aurora. [Abstracter's note: Complete translation]

Card 2/2

8(3)

AUTHORS: Mann, A. K., Candidate of Technical Sciences, SOV/105-59-7-15/30
Mironov, A. V., Engineer, Lemina, N. F., Engineer

TITLE: Detection of the Damaged Point in a Long Cable Line (Opredeleniye mesta povrezhdeniya kabel'noy linii bol'shoy protyazhennosti)

PERIODICAL: Elektrichestvo, 1959, Nr 7, pp 57 - 61 (USSR)

ABSTRACT: The detection of a damaged point in the cable insulation is usually effected in two stages: First, the distance to the damaged point is determined at the end of the line, and then the damaged point is located. At present, the problem of determining the distance to the faulty point is solved. At the Vsesoyuznyy nauchno-issledovatel'skiy institut elektroenergetiki (All-Union Scientific Research Institute for Power Engineering) devices of the types IKL and EMKS (Ref 1) were developed. The methods hitherto employed for the detection of faulty points - the induction- and the acoustic methods - have not been found satisfactory. Several new methods of detecting faulty points in the cable are described, which make it possible to detect a small zone in which the faulty point is located. Some consist in measuring the electromagnetic field, and others in measuring the

Card 1/2

Detection of the Damaged Point in a Long Cable Line SOV/105-59-7-15/30

current drop on the surface in the damaged zone. Among the first-mentioned are the induction- and pulse-induction methods, among the others, the contact- and pulse-contact methods. These four methods are described in this paper. The first two permit the determination of a small zone in the cable line: at a frequency of 10 megacycles this zone is about 60 m long, and at 50 megacycles its length is 10 - 15 m. The contact- and the pulse-contact methods make it possible, in the case of a uniform earth covering, to determine a small zone in the line and to detect the faulty point with an accuracy of up to ±1 m. The methods described may be used for the detection of faulty points in any type of cable with earthed metal envelopes. There are 6 figures and 3 Soviet references.

ASSOCIATION: Nauchno-issledovatel'skiy institut postoyannogo toka (Scientific Research Institute for Direct Current)

SUBMITTED: December 1, 1958

Card 2/2

MIRONOV, Aleksandr Yevgen'yevich; KANAYEV, Aleksey Pavlovich

[The republic's tomorrow; the story of the seven-year plan for developing the national economy of White Russia] Zavtrashnii den' respubliki; rasskaz o semiletnem plane razvitiia narodnogo khoziaistva Belorusskoi SSR. Minsk, Gos.izd-vo BSSR, 1959. 50 p. (MIRA 13:12)

(White Russia--Economic policy)

MIRON V. B A

BORISOVA, A.O.; BOCHANTSEV, V.P.; BUTKOV, A.Ya., dotsent; VASIL'KOVSKAYA, A.P.; VVEDENSKIY, A.I., dotsent; GOLODKOVSKIY, V.L.; GONCHAROV, N.F. [deceased]; DROBOV, V.P., professor; KOROTKOVA, Ye.Ye.; KOSTINA, K.F.; KUDRYASHEV, S.N. [deceased]; LAKHINA, M.M.; LINCHEVSKIY, I.A.; MIRONOV, B.A. [deceased]; PAZIY, V.K.; POYARKOVA, A.I.; PROTOPOPOV, G.F.; SUMNEVICH, G.P. [deceased]; KHAL'ZOVA, K.P.; YUZEPCHUK, S.V.; KOROVIN, Ye.P., professor, glavnyy redaktor; ZAKIROV, K.Z., professor, redaktor; SHIPUKHIN, A.Ya, redaktor izdatel'stva

[The glora of Uzbekistan] Flora Uzbekistana. Glav. red. E.P.Korovin. Tashkent, Izd-vo Akademii nauk UzSSR. Vol.3. 1955. 825 p. (MLRA 9:10)

1. Deystvitel'nyy chlen AN UzSSR (for Korovin)
(Uzbekistan--Botany)

MIRONOV, B.A.

Hydrological characteristics of forests in the Il'men' Preserve. Trudy Inst. biol. UFAN SSSR no. 25:33-45 '61. (MIRA 15:6
(Il'men' Preserve—Forest soils) (Soil moisture)

MIRONOV, S.A.

Practice in det[illegible] [illegible]
zones. Geol. [illegible]

135-6-7/13

SUBJECT: USSR/Welding.

AUTHORS: Zabetin, V.F., Engineer, Vychegzhanin, A.A., Engineer, and Mirenov, B.A., Technician.

TITLE: Introducing Semi-Automatic Welding in Carbon Dioxide Medium in Shipbuilding (Vnedreniye v sudostreyenii peluavtematicheskoy svarki v srede uglekislogo gaza).

PERIODICAL: "Svarochnoye Preizvodstve", 1957, # 6, pp 15-17 (USSR).

ABSTRACT: Experiments with the method have been started at the author's plant in 1955 and resulted in use of semi-automatic welding in carbon dioxide in the production of the plant. The automatic welding method remained in the laboratory due to lack of reliable equipment and the complexity of re-adjusting existing welding machines. However, replacing manual welding in shipbuilding by more efficient welding methods is a task of paramount importance.

The semi-automatic welding stand in use consists of the semi-automatic device "ПШ -5" (or "ПШ-500"), the holder of which has been replaced by a special gas torch, a carbon dioxide container with an attached electric heater, and a standard oxy-

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135-6-7/13

TITLE: Introducing Semi-Automatic Welding in Carbon Dioxide Medium in Shipbuilding (Vnedreniye v sudostroyenii poluavtomaticheskoy svarki v srede uglekislogo gaza).

gen reducer The gas driers "POK-1" recommended by "TsNIITMASh" were rejected since they contributed no improvement in work and caused freezing of reducer after 10-15 minutes. The author's plant designed a torch which differs from other designs (used in the Podol'skiy Plant imeni Ordzhonikidze and in the Nevskiy Machinebuilding Plant) by less weight and more handiness. It is cooled by the passing carbon dioxide, which simplifies welding. The torch is shown by drawings. The welding technology is given in the article. The method is being widely used in welding ship pipelines, parts of ship ventilation systems and superstructures. It is highly economical compared to manual welding.

The article contains 2 drawings, 1 set of sketches, 2 photographs, 1 table.

ASSOCIATION: Not stated.
PRESENTED BY:
SUBMITTED:
AVAILABLE: At the Library of Congress.

Card 2/2

ZABOTIN, V.G., inzhener; MIRONOV, B.A., inzhener.

Practices of gas cutting of parts with an MDFKS automatic machine.
Sudostroenie 23 no.3:45-47 Mr '57. (MLRA 10:5)
(Gas welding and cutting)

STETSENKO, I.P., inzh.; MIRONOV, B.A.

Screw press for toilet soap. Masl.-zhir. prom. 24 no.10: 39-41 '58. (MIRA 11:10)

1. Nevskiy mylovarennyy zavod.
(Power presses) (Soap)

Mironov, B.F.

USSR

Synthesis of diallylsilanes. A. D. Petrov, B. F. Mironov, and D. G. Glukhovtsev (*Izvest. Akad. Nauk S.S.S.R., Otdel. Khim. Nauk,* 1954, 6, 1123—1124).—Some new diallylsilanes were synthesised by suitable Grignard reactions. E.g. a mixture of ethyldichlorosilane (25·3 g.) and allyl iodide (100 g.) was added during 4 hr. to 20 g. of Mg in 250 ml. of ether. The reaction yielded *ethyldiallylsilane*, $C_8H_{16}Si$ (8 g.), b.p. 147·5°/740 mm., n_D^{20} 1·4510. Other compounds of this series were obtained in a similar way: *dimethyldiallylsilane*, $C_8H_{16}Si$ (77·5%), b.p. 135·5°/760 mm., n_D^{20} 1·4420; *diphenyldiallylsilane*, $C_{18}H_{20}Si$ (62%), b.p. 140·5°/2 mm., n_D^{20} 1·5750; *methyl(phenyl)diallyl silane*, $C_{13}H_{18}Si$ (73·2%), b.p. 212°/770 mm., n_D^{20} 1·5220; *α-naphthyl(methyl)diallyl silane*, $C_{17}H_{20}Si$ (53·2%), b.p. 140°/1 mm., n_D^{20} 1·5879. *α-Naphthyl(methyl)dichlorosilane*, $C_{11}H_{10}SiCl_2$, b.p. 122°/1 mm., n_D^{20} 1·6025, was obtained in 33·2% yield by interacting methyl trichlorosilane (480 g.) with α-naphthyllithium, prepared from 28·9 g. of Li and 416 g. of α-naphthyl bromide.

L. S.

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KRAVCHENKO, A.A., starshiy nauchnyy sotrudnik; MIRONOV, B.I.;
BALASHOV, V.I.

Vestibulometry and oxyhemometry in hypertensives. Trudy MONIKI no.5:115-131 '62. (MIRA 16:4)

1. Otorinolaringologicheskaya klinika Moskovskogo oblastnogo nauchno-issledovatel'skogo klinicheskogo instituta (direktor - zasluzhennyy deyatel' nauki, prof. I.Ya.Sendul'skiy).

(HYPERTENSION) (VESTIBULAR APPARATUS)
(BLOOD-OXYGEN CONTENT)

-6-

KALISHEVSKIY, L.L.; KATSNEL'SON, B.D.; KNORRE, G.F.; MIRONOV, B.M.; NADZHAROV, M.A.; NAKHAPETYAN, Ye.A.; SAKHAROV, V.M.; KHVOSTOV, V.I.; KORIKOVSKIY, I.K., red. izd-va; VORONIN, K.P., tekhn. red.

[Cyclone furnaces] TSiklonnye topki. Pod obshchei red. G.F. Knorre i M.A. Nadzharova. Moskva, Gos. energ. izd-vo, 1958. 215 p. (MIRA 11:7)
(Furnaces, Heat treating)

SOV/[illegible] /

AUTHOR: Mironov, [illegible], Engineer

TITLE: Thermal Characteristics of a Cyclone Furnace (Te[illegible] kharakteristiki tsiklonnoy topki)

PERIODICAL: Teploenergetika, 195[illegible], Nr [illegible], pp 3[illegible] - [illegible] (USSR)

ABSTRACT: Experimental equipment was used to evaluate the fundamental thermal characteristics of cyclone furnaces [illegible] solid fuel. Data were collected on direct heat-[illegible] the cyclone, on mechanical and chemical under-burning [illegible] on the specific thermal loading of the furnace [illegible] together with investigations of the aerodynamics [illegible] the fields of temperature and volume and [illegible] in the liquid slag film; the data provide a basis for the thermal design of a cyclone chamber.

The experimental equipment and procedure have been described elsewhere. Calorimetric data on the cyclone and combustion chamber were used to determine the direct heat-emission and thermal loading. The experimental [illegible] is illustrated schematically in Figure 1A. [illegible] was introduced [illegible] axially.

In evaluating the operation of the actual furnace [illegible] advisable to relate the combustion component of the furnace heat-balance to the total quantity of heat [illegible]

Card 1/[illegible]

SOV/[illegible]/

Thermal Characteristics of a Cyclone Furnace

furnace and not to the calorific value of the fuel [illegible] determination of the direct heat output and specific thermal loading of the heating surface is described. The gas temperature at the outlet from the combustion chamber was calculated from the heat balance. In calculating the gas temperature at the outlet from the cyclone into the combustion chamber it was assumed that the under-combustion [illegible] combustion chamber is equal to that beyond the cyclone. The following constructional elements of the cyclone were changed during the experiments: the shape of the front [illegible] the diameter of the outlet nozzle, the location [illegible] secondary air and the length of the cyclone. Detailed information about these changes is given. The secondary air nozzle was initially [illegible] the cyclone but was gradually moved into the cyclone. I[illegible] combustion took place at the back of the cyclone [illegible] than 30-40% of the heating surface was covered with [illegible]. However, as the secondary air nozzle was moved into the [illegible] the whole cyclone became filled with flame and all the [illegible] surface was covered with slag. The res[illegible] the heating surface rose from 80 to 150 x 10^3 kcal/m[illegible]

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SOV/96-58-[illegible]

Thermal Characteristic of a Cyclone Furnace

data on the increased thermal loading are given in Table 1. Lengthening of the cyclone did not change the general process of combustion but halved the under-combustion. The other alterations in constructional elements of the cyclone made little difference to its operation. The rate of primary air introduction was varied from 1[illegible] to 250 m/sec., but this increased the tangential velocities by not more than 4%. Moreover, as shown by Figure 2, the gas/air mixture moving near the wall has a temperature close to that of the liquid slag. Other things being equal, change in the rate of air delivery to the cyclone did not increase the thermal loading of the furnace, as will be seen from Figure 3. Therefore, convection has negligible influence on the thermal loading of cyclone heating surfaces covered with liquid slag. The rate of fuel delivery was varied from 250-480 kg/hr. In itself, this had no influence on the specific thermal loading of the cyclone (see Figure 3), perhaps because of back radiation from the film of hot slag and similar factors. Increase in the quantity of primary air improves the way in which the chamber is filled with flame and increases the extent to which the heating surface of the cyclone is covered

Card3/6

Thermal Characteristic of a Cyclone Furnace [illegible]

with liquid slag. As Figure 3 indicates, a higher air temperature increases the specific thermal loading. The complexity of the system (the film of moving liquid slag, the solid slag, the lining and metal walls) [illegible] has an effect upon the thermal loading of the heating surfaces. For instance, the influence of the lining [illegible] specific thermal loading can be seen from Table [illegible]. The article then [illegible] the design of a furnace with cyclone chambers. The three-chamber cyclone furnace illustrated in Figure [illegible] is the most widely used type. The first chamber is the [illegible] the second is the [illegible] in which the combustion should be completed; the third [illegible] cooling chamber does not function strictly as a furnace but rather as a heat-exchanger of the radiation type. The factors that promote complete combustion are then discussed and the process is compared with that in [illegible]. In the three-chamber furnace, the primary [illegible] lation of radiated heat-exchange is then considered. [illegible] cooling chamber can be designed on the basis of the [illegible] flux of the gas, and the combustion chamber likewise provided the excess-air factor is not great. The primary heat emission [illegible]

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Thermal Characteristic of a Cyclone Furnace SOV/[illegible] /

of the cyclone, or the mean specific thermal loading of the screens, can be calculated independently of the other furnace chamber. However, the usual form of thermal calculation of furnaces must be revised because of the very high temperature level in cyclone furnaces. There is still no published Soviet or foreign work on heat exchange in combustion and cooling chambers and the author's own ideas on this subject are incomplete. Nevertheless, the primary evaluation of the thermal characteristics of closed-type cyclone furnaces can now be made with reasonable reliability, using the recommendations made here in conjunction with standard furnace design procedure.

The calculation of heat exchange in the cyclone chamber is then considered. A formula has been recommended for this purpose but its limitations are pointed out and the results of recent work by A.M. Gurvich are used to derive a more widely applicable expression for determining the mean specific thermal loading of the heating surfaces, which may be used to calculate local heat absorption in a cyclone furnace. An expression is also give for the gas temperature at the outlet from the cyclone. The results of these calculations are

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SOV/[illegible]

Thermal Characteristic of a Cyclone Furnace

represented graphically in Figure 4. The coefficient of the temperature field, calculated as a function of the thermal loading, is plotted in Figure 5. Finally, a procedure is recommended for making calculations of heat exchange in a cyclone furnace with liquid ash removal and axial introduction of pulverised fuel. The results given in Figure 6 show that theory and practice are in good agreement. There are 6 figures, 2 tables and 9 references, [illegible] of which are Soviet and 1 German.

ASSOCIATION: **Moskovskoye** vyssheye tekhnicheskoye uchilishche (Moscow Higher Technical College)

Card 6/6

1. Furnaces--Theraml properties 2. Furnaces--[illegible] 3. Fuels--Applications

MIRONOV, B.M., inzh.

Thermal characteristics of a cyclone furnace. Teploenergetika 5 no.5:38-43 My '58. (MIRA 11:5)

1.Moskovskoye vyssheye tekhnicheskoye uchilishche.
(Furnaces)

MIRONOV, B.M., inzh.

Heat transfer in a test cyclone furnace with hydraulic clinker removal. [Trudy] MVTU no.94:145-163 '58. (MIRA 12:3)
(Combustion) (Furnaces)

VASILENKO, Aleksey Nikolayevich, kand. tekhn. nauk; [illegible], Yevgeniy Vasil'yevich, dots.; ISAYEV, Sergey Ivanovich, kand. tekhn. nauk; [illegible], Nikolay Karpovich, kand. tekhn. nauk, dots.; [illegible], Vyacheslav Ivanovich, assistent; K[illegible], Vitaliy Ivanovich, dokt. tekhn. nauk, prof.; MIRONOV, Boris Mikhaylovich, kand. tekhn. nauk; NIGMATULIN, Iskander Nigmatullovich, doktor tekhn. nauk, prof.; NOSOV, Mikhail Vasil'yevich, prof.; SA[illegible], [illegible] Sergeyevich, assistent; [illegible], Igor' Pavlovich, kand. tekhn. nauk, prof.; [illegible], Viktor Ivanovich, kand. tekhn. nauk; SHISHOV, Yevgeniy Viktorovich, kand. tekhn. nauk; [illegible], Boris Nikolayevich, kand. tekhn. nauk, [illegible]; [illegible], kand. tekhn. nauk, [illegible]; SHVE[illegible], dots., retsenzent; [illegible]TSINA, [illegible]; [illegible]TAYEVA [illegible].

[illegible] in technical thermodynamics and heat [illegible]; Sbornik zadach po tekhnicheskoy termodinamike i teploperedache. [By] A.N.Vasilenko i dr. Moskva, [illegible] [illegible] (MIRA [illegible]) [illegible] 309 p.

.. Prepodavatel'skiy kollektiv kafedry termodinamiki i teploperedachi [illegible] vysshego tekhnicheskogo [illegible] (for all except Kutyrin, Shishov, [illegible]). [illegible]kovskiy aviatsionnyy institut (for Kutyrin, [illegible]).

L 10632-66 EWT(m)/EWP(w)/T/EWP(t)/EWP(b)/EWA(c) IJP(c) JD/JG

ACC NR: AR5023519 SOURCE CODE: UR/0275/65/000/008/A013/A013

SOURCE: Ref. zh. Elektronika i yeye primeneniye, Abs. 8A85

62
B

AUTHOR: Aleksandrov, L. N.; Mironov, B. N.; Zvereva, T. M.

TITLE: Investigation of tungsten recrystallization upon quick electric heating

CITED SOURCE: Uch. zap. Mordovsk. un-t, vyp. 36, 1964, 53-57

TOPIC TAGS: tungsten filament, tungsten, metal recrystallization, tensile strength, annealing

TRANSLATION: Prior to annealing, the specimens were cleaned by boiling in a 20% solution of NaOH for 10 min. The recrystallization process was studied by the variation of the ultimate strength at room temperature with the annealing temperature and time. The ultimate strength was determined on a RM-05 tensile testing machine. For an annealing time of 30 min, the final primary-recrystallization temperature was about 1450C; for 10 min, almost 1520C; and for 200 sec, 1600C. From the above data, a curve of primary-recrystallization-completion time vs. annealing temperature was plotted. A metallographic method corroborated the fact that the recrystallization goes quicker with higher rates of heating. Bib 4.

SUB CODE: 11, 20, 13

Card 1/1 UDC: 621.52:669

DOLGOPOLOV, Konstantin Vasil'yevich; FEDOROVA, Ye.F.; MIRONOV, B.P.;
ANISHCHENKO, K.A.; POKSHINSEVSKIY, V.V., otv. red.; LYUBIMOV,
I.M., red.; KONOVALYUK, I.K., mladshiy red.; KISELEVA, Z.A.,
Z.A., red. kart; VILENSKAYA, E.N., tekhn. red.

[Central Black Earth Region; economic and geographical
characteristics] TSentral'no-chernozemnyi raion; ekonomiko-
geograficheskaia kharakteristika. Moskva, Gos. izd-vo geogr.
lit-ry, 1961. 414 p. (MIRA 14:10)
(Central Black Earth Region—Geography, Economic)

MIRONOV, B.P.

Unique model of a globe. Geod.i kart. no.7:72-76 Jl '62. (MIRA 15:8)

(United States--Globes)

MIRONOV, B.P.

21

2669. EXPERIMENTAL INVESTIGATION OF TEMPERATURE FIELDS IN THE AUSTENITE BODY OF A GAS TURBINE UNDER STEADY AND STARTING CONDITIONS. Mironov, B.P. (Izv. Akad. Nauk SSSR, Otdel. Tekh. Nauk (Bull. Acad. Sci. U.S.S.R., Sect. Tech. Sci.), Sept. 1956, 31-38). Experiments with 164 thermocouples installed on a 1 MW gas turbine are recorded.

SH

MIRONOV, B. P. Cand Tech Sci -- (diss) "Study of the convective heat absorption of immobile screens placed at ~~the~~ ends of rotating gas-turbine **vanes**." Len, 1959. 19 pp (Len Shipbuilding Inst), 150 copies (KL, 48-59, 115)

S/024/60/000/03/016/026
E081/E441

AUTHOR: Mironov, B.P. (Leningrad)

TITLE: Investigation of Convective Heat Exchange in Screens Fixed at the End of a Rotating Disk

PERIODICAL: Izvestiya Akademii nauk SSSR Otdeleniye tekhnicheskikh nauk Energetika i avtomatika, 1960, Nr 3, pp 129-137 (USSR)

ABSTRACT: A longitudinal section through the experimental
arrangement is shown in Fig 1 (1 - packing,
2 - hot housing, 3 - technically smooth disk,
4 - electric heater, 5 - cooling device, 6 - bearing
cover, 7 - heat insulating case, 8 - packing,
9 - asbestos packing, 10 - ring-calorimeters,
11 - bush, 12 - packing, S - clearance). Opposite the
smooth surface of the disk, which was rotated at speeds
of 200 to 3700 rpm, were six concentric ring calorimeters
forming a water screen. The temperature of the water
entering and flowing out of the calorimeters was measured
with a mercury thermometer. The air temperature in the
space between the disk and screen was measured with a
system of nichrome-constantan thermocouples. The
distribution of air velocity in the space was also

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S/024/60/000/03/016/028
E081/E441

Investigation of Convective Heat Exchange in Screens Fixed at the End of a Rotating Disk

measured. The experimental data on heat emission were dealt with in terms of the similarity criteria Nu and Re (foot of p 130) where α_i is the local value of the heat emission coefficient at the i-th calorimeter (equation at the top of p 131) $Q_1 = Gc\Delta t$ is the quantity of heat taken up by the calorimeter, G is the flow of water through the calorimeter, c is the heat capacity of the water, Δt is the difference in temperature between entrance and exit. F_1 the area of heat absorbing surface of the calorimeter facing the disk t_k its temperature. t_s the air temperature in the middle of the space. ω the angular velocity of the disk R_1 the mean radius of the calorimeter. λ ν are constants of the air at temperature t_s °C The heat absorption of the screen by convective heat exchange is described by the Eq (2.1) (Fig 2 Heat absorption of the screen: a - in the absence of air flow but without dividing the heat into radiation and convection components, б - in the absence of air flow heat received

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S/024/60/000/03/016/028
E081/E441

nvestigation of Convective Heat Exchange in Screens Fixed at the
nd of a Rotating Disk

by convection B - with air flow but without dividing heat into radiation and convection components (1) flow towards the centre (2) flow from the centre. Rm is the disk radius.) Values of m in (2.1) are given in Table 1. Fig 3 shows the change in total velocity of flow with width of space (a - in the absence of through flow. б with through flow towards the entre B - with through flow away from the centre) Rapid change of velocity is only observed near the disk and screen Fig 4 shows the change in total velocity of motion at the middle of the space with kinematic factor $1/K_w$ (foot of p 132) a - with flow towards the centre б with flow from the centre. For pure convective flow the equation (3.1) holds, with φ as defined in the middle of p 134 and tabulated in Tables 2 and 3 Fig 5 shows the relation between the coefficient a (foot of p 134) and $1/K_w$ for different values of the spacing S and radius R_1 and in

Card 3/4

Vc

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E081/E441

Investigation of Convective Heat Exchange in Screens Fixed at the End of a Rotating Disk

Fig 6 a is shown as a function of $S/(R_1 - R_B)$ and $1/K_w$ (R_B is the radius of the shaft). Fig 7 gives the change in velocity of motion of the nucleus of flow (in the middle of the space) in the absence of air flow with width of space. There are 7 figures 3 tables and 9 references 7 of which are Soviet and 2 English

SUBMITTED: Arpil 10 1959

Card 4/4

✓C

MIRONOV, Boris Petrovich; LEVCHENKO, Ya.V., inzh., red.; SHILLING, V.A., red. izd-va; GVIRTS, V.L., tekhn. red.

[Inclined tubular kiln for burning vermiculite]Trubchataia naklonnaia pech' dlia obzhiga vermikulita. Leningrad, 1962. 12 p. (Leningradskii dom nauchno-tekhnicheskoi propagandy. Obmen peredovym opytom. Seriia: Stroitel'naia promyshlennost', no.23)

(Vermiculite) (Kilns) (MIRA 16:2

KUTATELADZE, S.S.; LEONT'YEV, A.I.; [illegible], [illegible].A.; [illegible], E.I.; [illegible].A., [illegible]; [illegible], [illegible].A.; [illegible]LLOVA, [illegible]; [illegible], [illegible]; [illegible]ZHIN, [illegible].A.; [illegible]; [illegible], V.A.; [illegible]KHINA, [illegible]; FEDOROV, V.K.; [illegible]A.AKHMA[illegible]EVA, Y[illegible]; [illegible], A.[illegible]; SHIAKOVSKAYA, L.I., red.

[Heat and mass transfer and friction in a turbulent boundary layer] Teplomassoobmen i trenie v turbulentnom pogranichnom sloe. Novosibirsk, Red.-izd. otdel Sib. otd-niia AN SSSR, [illegible] p. [illegible] A [illegible])

S/114/62/000/007/002/003
E194/E455

AUTHORS: Kuznetsov, L.A., Candidate of Technical Sciences,
Mironov, B.P., Candidate of Technical Sciences

TITLE: Internal thermal insulation of the casing of gas turbine type ГТ -700-5 (GT-700-5)

PERIODICAL: Energomashinostroyeniye, no.7, 1962, 23-26

TEXT: Gas turbines operate with an inlet gas temperature of 700°C or more and so special precautions are required in the design of casing. The earlier solution was to use austenitic steels but these have various disadvantages. Air cooling is quite effective but is difficult to distribute uniformly and there is some loss of efficiency. Internal thermal insulation give good results and casing temperatures can thereby be much reduced. It has the disadvantage of requiring a larger casing and, moreover, local cooling may still be required at places where there is direct thermal contact between the frame and hot parts. The properties required of internal thermal insulation are

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E194/E455

Internal thermal insulation ...

discussed; of available materials the most suitable are kaolin wadding and fibrous alumina. Since 1955, the Nevskiy mashinostroitel'nyy zavod (Nevsk Engineering Works) has used vermiculite concrete as thermal insulation of full-scale and model gas turbines. The composition of this material is described. Tests showed that it needed air gaps to allow for thermal expansion. Three prototypes of turbine type GT-700-5 were internally insulated with vermiculite concrete, micro-slag wadding grade M-100, and an experimental batch of kaolin fibre. The construction of the internal insulation, particularly that of vermiculite concrete, is described in some detail. Graphs of steady temperature against gas inlet temperature for different parts of the turbine show in particular that the centre part of the casing could be kept to about 400°C with inlet gas temperature of 700°C. Graphs also show changes of temperature with time for various parts of the turbine; the casing heated up steadily for a period of 5 to 6 hours. After 230 hours operation and 60 starts the kaolin and slag wadding insulation of the first machine showed no obvious shrinkage. The appearance of the kaolin wadding was

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Internal thermal insulation ... S/114/62/000/007/002/003
E194/E455

unaltered whilst the slag wadding had become more brittle and broke up more easily. The results so far available do not permit of a firm choice between kaolin wadding or vermiculite concrete. Present indications are that high-temperature wadding is preferable to the concrete and insulation of this kind protected with heat-resisting fabric does not require air gaps, does not shrink and is of very uniform properties over its entire area. There are 6 figures.

Card 3/3

L 5395-66
WW/DJ EWT(l)/EWP(m)/EWT(m)/EPF(c)/ETC/EPF(n)-2/EWG(m)/EWA(d)/T/FCS(k)/EWA(l)

ACC NR: AP5027289

SOURCE CODE: UR/0207/65/000/005/0162/0166

AUTHORS: Leont'yev, A. I. (Novosibirsk); Mironov, B. P. (Novosibirsk)

4

ORG: none

TITLE: Extension of limiting relative friction and heat transfer laws to nonisothermal gas flows with finite Reynolds numbers

SOURCE: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 5, 1965, 162-166

TOPIC TAGS: heat transfer, skin friction, Reynolds number, gas flow, turbulent boundary layer

ABSTRACT: The skin friction and heat transfer data in the literature are reviewed in detail to show that limiting friction and heat transfer laws, calculated theoretically, are also applicable to nonisothermal flows with finite Reynolds numbers. This is shown to be possible if local skin friction coefficients C_{f_0} and local Stanton numbers S_0 are defined. For example, an excellent data correlation is obtained with the expression

$$C_{f_0} = 0.0252 (R^{**})^{-0.25}$$

Card 1/2

L 5395-66
ACC NR: AP5027289

where the Reynolds number is defined by the local parameters

$$R^{**} = \frac{w_0 \rho_0 \delta^{**}}{\mu_w}.$$

A similar agreement with experimental data is obtained with the limiting equations

$$\Psi_w = \left(\frac{2}{\psi^{0.5}+1}\right)^2$$

where

$$\Psi = \frac{C_f}{C_{f_0}}$$

$$\psi = \frac{T_w}{T_w^*}.$$

Thus, the introduction of C_{f_0} in the ratio Ψ allows one to calculate nonisothermal turbulent boundary layers from the limiting expressions for Ψ without including the effects of finite Reynolds numbers. The same procedure can be followed for the heat transfer laws. A brief explanation is given to show that this behavior is intuitively obvious. Orig. art. has: 8 formulas and 2 figures.

SUB CODE: ME/ SUBM DATE: 20Sep64/ ORIG REF: 007/ OTH REF: 022

Card 2/2

L 27160-66 EWT(1)/EWP(m)/EWA(1) WW

ACC NR: AP6012672

SOURCE CODE: UR/0170/66/010/004/0447/0451

AUTHOR: Leont'yev, A. I.; Mironov, B. P.; Lugovskoy, P. P.

ORG: Institute of Thermophysics of the SO, AN SSSR, Novosibirsk (Institut teplofiziki SO AN SSSR)

42
B

TITLE: Experimental determination of the critical blowing parameter on a porous plate

SOURCE: Inzhenerno-fizicheskiy zhurnal, v. 10, no. 4, 1966, 447-451

TOPIC TAGS: turbulent boundary layer, blowing parameter, porous plate

ABSTRACT: Experimental data on the determination of the critical blowing parameter on a porous plate are given. The method is based on the chemical reaction of the main stream with the fluid injected. The main stream is an acid solution and the injected fluid is an alkali solution colored by phenolphthalein. With injection flow rates below critical, a neutralization reaction takes place which results in decoloration of phenolphthalein. At critical injection flow rates, the main stream is displaced, and a clearly distinguishable film of the injected liquid appears on the plate surface. The experimental values of the critical injection parameter are in good agreement with the predicted ones obtained by the asymptotic theory of the turbulent boundary layer. Orig. art. has: 3 figures, 3 formulas, and 1 table. [NT]

SUB CODE: 20/ SUBM DATE: 08Aug65/ ORIG REF: 002/ OTH REF: 004/

Card 1/1

UDC: 532.526

[illegible] EWT(1)/[illegible] EWP(m)/EWP(v)/[illegible](f)/ EWP(v)/ EWP(k) IJP(c) [illegible]

SOURCE CODE: [illegible]/0207/66/000/004/0116/0120

[illegible]

ORG: none

TITLE: Calculation of heat transfer in nozzles

SOURCE: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 4, 1966, 116-120

TOPIC TAGS: nozzle, nozzle [illegible], [illegible] propulsion, jet propulsion, rocket propulsion, supersonic nozzle, heat transfer coefficient

ABSTRACT: A simplified method has been developed for calculating the heat transfer coefficient in subsonic and supersonic nozzles. The method, which is based on the solution of the energy equation, uses the parameter Ψ which is defined as the ratio of the Stanton number St under the flow conditions studied to the St on a flat plate at an identical value of R_T^{**}, where

$$R_T^{**} = \frac{\delta_T^{**} w_0 \rho_0}{\mu_0};$$

δ_T^{**} is the thickness of the thermal boundary layer; w_0 and ρ_0 are the velocity and the density at the outer surface of the boundary layer, respectively; and μ_0 is the viscosity at the stagnation temperature, but in the absence of perturbations.

Card 1/2

L 08949-67

ACC NR: AP6030929

A formula was derived for the heat transfer coefficient in terms of Ψ and other flow parameters as a function of the position on the nozzles contour which was divided into several conical sections. The heat transfer coefficients obtained by the present method agreed closely with results obtained by exact integral relationships and from experiments. The results also showed that the ratio of the wall to the free stream temperature Ψ has a neglibible effect on Ψ. In the supersonic section, however, (at $\Psi < 1$) due to the effect of Ψ, Ψ varies from 1.1 to 1.3. The function Ψ can be also used for calculating the heat transfer in nozzles during nonsteady-state flow or at variable wall temperatures. Orig. art. has: 5 figures and 12 formulas.

[PV]

SUB CODE: 21,20/ SUBM DATE: 06Jul64/ ORIG REF: 004/ OTH REF: 006/

ACC NR: AP7000[illegible]   SOURCE CODE: UR/0207/66/0[illegible] [illegible]/0123/0129

AUTHOR: Kutateladze, S. S. (Novosibirsk); Leont'yev, A. I. (Novosibirsk); Mironov, B. P. (Novosibirsk)

ORG: none

TITLE: Calculation of turbulent heat transfer on a semipermeable surface with injection of foreign gas

SOURCE: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no.5,1966, 123-129

TOPIC TAGS: turbulent heat transfer, semipermeable surface, sweat cooling, subsonic flow

ABSTRACT: A method is presented for calculating the heat transfer on a semipermeable surface under conditions of subsonic flow with foreign gas injection. The method is based on the solution of the energy equation and the use of the asymptotic theory of the turbulent boundary layer. Figure 1 shows the comparison of the calculated results with experimental data obtained by Tefik, Eckert, et al. (Thermal diffusion effects on energy transfer in turbulent boundary layer with helium injection. Proc. of the 1962 heat transfer and fluid. Mechanics Institute, Stanford University Press, 1962).

Card 1/3

ACC NR: AP7000058

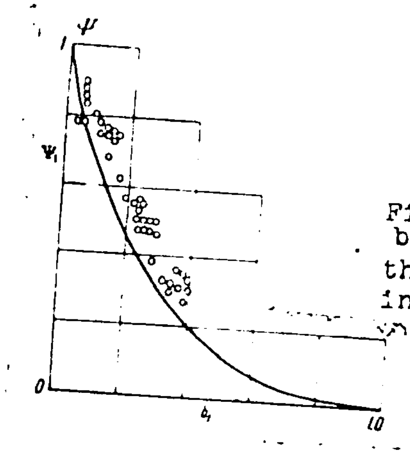

Fig.1. Variation of ψ_1 with b_1 (ψ_1 - function of the Stanton numbers; b_1 injection parameter.

Figure 2 shows the rate of gas injection for the case where c_p is different for the injected and main gases.

Card 2/3

ACC NR: AP7000058

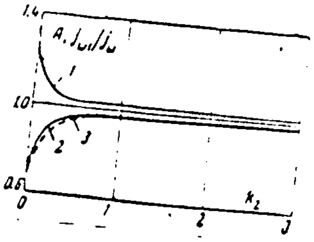

Fig.2. Variation of [illegible] with k_2. (j_w - rate of gas injection)

The calculation was performed for: k_2=0.005--6.0; R=0.25; c_{p1}/c_{p0}= 0.25; γ=0.303--0.9, where k_2 is a function of the wall and gas temperatures, and c_{p0} and c_{p1} are the specific heats of the main and injected gases, respectively. The obtained results show that the rate of injected gas is only slightly affected by the physical properties of injected and main gases. Orig.art.has: 2 figures and 20 formulas.

[WA-88]

SUB CODE: 21/ SUBM DATE: 06Aug65/ ORIG REF: 001/ OTH REF: 001

Card 3/3

L 62705-65 EWP(m)/EWT(l)/FCS(k)/EWA(l) Pd-1/Pi-4 WW

ACCESSION NR: AP5020208 UR/0170/65/009/001/0003/0008
532.536

26
25
B

AUTHOR: Mironov, B. P.

TITLE: Turbulent boundary layer in a supersonic diffuser.

SOURCE: Inzhenerno-fizicheskiy zhurnal, v. 9, no. 1, 1965, 3-8

TOPIC TAGS: boundary layer theory, turbulent boundary layer, supersonic diffuser, friction coefficient

ABSTRACT: The problem of calculating the turbulent boundary layer of a compressible gas in a supersonic diffuser at a positive longitudinal pressure gradient is analyzed. The proposed one-parameter method for calculating the local friction coefficient under isothermal conditions C_f, the shape parameter H, and the momentum thickness δ^{**} is based on the theory of limiting laws. (Kutateladze S. S., Leont'yev, A. I. Turbulentnyy pogranichnyy sloy szhimaemogo gaza. Izd. SO AN SSSR, Novosibirsk, 1962.) The values of C_f, H, and δ^{**} obtained by the proposed method were compared with previously published experimental and theoretical values and were found to be very satisfactory. Orig. art. has: 4 figures and 6 formulas. [PS]

Card 1/2

L 62705-65

ACCESSION NR: AP5020208

ASSOCIATION: Institut teplofiziki SO AN SSSR, Novosibirsk (Institute of Thermophysics, SO AN SSSR)

SUBMITTED: 30Oct64 ENCL: 00 SUB CODE: ME

NO REF SOV: 007 OTHER: 007 ATD PRESS: 4064

Card 2/2

MALYSHEV, I.F.; POPKOVICH, A.V.; ROSHAL', G.Ya.; ZHELEZNIKOV, F.G.;
LYSOV, A.V.; TSEPAKIN, S.G.; SOLNYSHKOV, A.I.; BOYTSOV, A.S.;
ASTAKHOV, Ye.Ya.; MIRONOV, B.V.; LAPITSKIY, Yu.Ya.;
GATALIN, V.A.; KHOROSHKOV, V.S.

Electrostatic accelerator-injector in a proton synchrotron.
Prib. i tekh. eksp. 7 no.4 37-45 Jl-Ag '62. (MIRA 16:4

1. Nauchno-issledovatel'skiy institut elektrofizicheskoy apparatury Gosudarstvennogo komiteta po ispol'zovaniyu atomnoy energii SSSR i Institut teoreticheskoy i eksperimental'noy fiziki Gosudarstvennogo komiteta po ispol'zovaniyu atomnoy energii SSSR.

(Particle accelerators) (Synchrotron)

L 42024-65 EWT(d)/EWT(1)/EEC(f)/EED-2/EWA(h)/EWP(1) Pg-4/Pi-4/Pk-4/Po-4/Pq-4/
Peb IJP(c) GG/BB

ACCESSION NR: AP5010947 UR/0286/65/000/007/0131/0131

AUTHORS: Yakubovich, A. M.; Korol'kov, I. V.; Braslavskiy, D. A.; Bubnov, I. A.; Mironov~~, B. V.~~

47
46
B

TITLE: Operational amplifier. 25 Class 42, No. 169878

SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 7, 1965, 131

TOPIC TAGS: amplifier

ABSTRACT: This Author Certificate presents an operational amplifier with parallel amplification channels and with automatic compensation of zero drift. To increase its reliability and accuracy of operation, it contains no less than three amplification channels operating alternately so that at any instant of time two of them are in the amplification mode. Each channel contains a dc amplifier with operation periodization and with discrete-periodic zero drift compensation by a circuit with a storage capacitor. To decrease the effect of a constant spurious signal with the breakdown of one of the channels, each channel contains a decoupling capacitor connecting the amplifier output of the particular channel through a resistance and a switching unit to the common output of the operational amplifier. The switching unit discharges the decoupling capacitor in the zero drift compensation mode.

Card 1/2

L 42024-65

ACCESSION NR: AP5010947 1

ASSOCIATION: Organizatsiya gosudarstvennogo komiteta po aviatsionnoy tekhnike (Organization of the State Committee for Aviation Technology)

SUBMITTED: 06Feb64 ENCL: 00 SUB CODE: EC

NO REF SOV: 000 OTHER: 000

Card 2/2

[illegible]

MIRONOV, P. K., Eng.

Automatic Control

Simplified scheme for automatizing the combustion process. Elek. sta., 23, No. 5, 1952.

Monthly List of Russian Accessions, Library of Congress, October 1952 UNCLASSIFIED.

MIRONOV, D.K.; PONOMAREVA, L.K., redaktor; LAPRUN, K.I., tekhnicheskiy redaktor

[Automatic control in electric power stations; the experience of electric stations of the Molotov power system in automatization of thermal processes] Avtomatika na elektrostantsiiakh; iz opyta avtomatizatsii teplovykh protsessov na elektrostantsiiakh Molotovenergo. Molotov, Molotovskoe kn-vo, 1955. 94 p. (MLRA 9:9)

1. Nachal'nik sluzhby naladki avtomatiki i teplovykh izmereniy (SNATI) Molotovenergo (for Mironov)
(Automatic control) (Electric power plants)

ACCESSION NR: AP4029217

S/0114/64/000/004/0030/0033

AUTHOR: Zaydman, M. Ye. (Engineer); Mironov, D. K. (Engineer)

TITLE: Operating experience with austenitic-steel steam superheaters of 180-atm, 565-580C steam boilers

SOURCE: Energomashinostroyeniye, no. 4, 1964, 30-33

TOPIC TAGS: superheater, steam superheater, boiler, steam boiler, 180 atm boiler, 565-580C steam boiler

ABSTRACT: Eight high-pressure boilers have been in operation at the Cherepet power station for 5-11 years. The superheaters of nos. 1-5 boilers are made from 1Kh14N14V2M steel; those of nos. 6-8 boilers, from 1Kh18N12T steel; the input coils of the superheaters of nos. 7 and 8 boilers are made from 12Kh1MF steel. The total number of faults in the superheater (32 mm, 5.5-mm wall) pipes has been about 440 as of 01Jan64. Nature of faults: bend cracks, straight-section

Card 1/2

ACCESSION NR: AP4029217

cracks, blows and breaks, weld cracks, others. The causes of the faults have been found: straight-section cracks were due to defective pipes (nonmetallic inclusions); bend cracks were due to cold-bending metal hardening (austenization and modification of the coil fastening cut the number of faults of this type from 49 in 1954 to 3 in 1962); blows and breaks were due to the creep of 1Kh18N12T steel under high-temperature (estimated as high as 680C) conditions. The superheater of no. 5 boiler after austenization and improving the pipe fastenings has operated reliably for 40,000 hrs. Orig. art. has: 5 figures and 1 table.

ASSOCIATION: none

SUBMITTED: 00

DATE ACQ: 01May64

ENCL: 00

SUB CODE: MM, PR

NO REF SOV: 002

OTHER: 000

Card 2/2

DIREKTOR, B.Ya., inzh.; LOSHAK, S.B., inzh.; MIRONOV, D.K., inzh., POLUKHIN A.I., inzh.

First results of the preliminary starts and operation of a 300 Mw. block. Elek. sta. 36 no.6:2-9 Je '65. (MIRA 18:7)

MIRONOV, Dmitriy Maksimovich; BUYANOVSKIY, N.I., redaktor; SAVINA, Z.A., vedushchiy redaktor; SHIKIN, S.T., tekhnicheskiy redaktor

[Operating and repairing turbodrills; work practice of the No.1 Drill Section of the Tuimazaburneft' Trust] Ekspluatatsiia i remont turboburov; opyt raboty kontory bureniia No.1 tresta Tuimazaburneft'. Moskva, Gos. nauchno-tekhn. izd-vo neftianoi i gorno-toplivnoi lit-ry, 1956. 50 p.

(Turbodrills) (MLRA 9:12)

MIRONOV, D.M.; SAFIULLIN, Kh.A.

What were the results of using water instead of drilling mud. Neftianik 1 no.1:10-11 Ja '56.
(MIRA 9:7)

1.Glavnyy inzhener kontory bureniya No.1 tresta Tuymazaburneft' (for Mironov).2.Nachal'nik planovogo otdela kontory bureniya No.1 tresta Tuymazaburneft' (for Safiullin).
(Oil well drilling fluids)

MIRONOV, D.M.

[illegible]. Water as drilling fluid. D. M. Mironov et al. Nafta (Krakow), 1956, 12, 248-9.—Excellent results were obtained in Bashkiria in 1952 using a turbo-drill and water in place of mud, and since then 880 m/rig/month have been reached in 1954. Theoretically it should be possible to reach 1500 m/rig/month in this way, which is also much cheaper and less corrosive. However, just before the oil-bearing formation is reached a change to ordinary mud is advised. M. S.

MIRONOV, D.M.

Completion of wells in bottom water drive type reservoirs.
Neftianik 6 no.1:8-10 Ja '61. (MIRA 14:4)

1. Glavnyy inzhener kontory bureniya No.1 tresta Tuymazaburneft'.
(Oil fields--Production methods)

MIRONOV, D.P.

Spectral determination of traces of silicon and certain cations in cellulose and its ethers. Zav.lab. 29 no.4:438 '63. (MIRA 16:5)

1. Vladimirskiy nauchno-issledovatel'skiy institut sinteticheskikh smol.

(Silicon—Analysis) (Cellulose—Spectra)

MIRONOV, D.P.; ZHARKOV, ..V.

Analysis of mixtures of [illegible] and anhydrides from their Raman spectra. Zav.lab. 29 no.12:[illegible]-1443 '63. (MIRA 17:1)

1. Vladimirskiy nauchno-issledovatel'skiy institut sinteticheskikh smol.

MIRONOV, D.P.; KHIN, N.N.; [illegible], V.V.; [illegible], M.V.;
SHULAYEV, N.P.

Preparation of butyric anhydride by the reaction of butyric acid with acetic anhydride in a continuous fractionating column. Zhur. prikl. khim. 38 no.10:2310-2312 O '65. (MIRA 18:[illegible])

1. Vladimirskiy nauchno-issledovatel'skiy institut sinteticheskikh smol. Submitted Sept. 3, 1963.

[illegible]: [illegible], [illegible] [illegible], [illegible]

[illegible]: [illegible]

[illegible]: [illegible]

[illegible]: [illegible] contained in the air [illegible] [illegible] and [illegible] as an internal standard [illegible]. The increase [illegible] analysis [illegible] of the "foreign" [illegible] that [illegible] with [illegible]. The air humidity has practically no influence on the "[illegible]" concentration.

[Abstracter's note: Complete translation] L. Vorob'yeva

Card 1/1

VOROB'YEV, S. A.; MIRONOV, [illegible]

Possibility of maintaining the blast conditions of a blast furnace at the optimum level. Izv. vys. ucheb. zav.; chern. met. 7 no.6:191-198 '64. (MIRA [illegible])

1. Ural'skiy politekhnicheskiy institut.

[illegible]

Electric [illegible] device for quality testing. [illegible]
no.9:1143-1144 '64. [illegible]

1. Ural'skiy politekhnicheskiy institut imeni [illegible].

[illegible]

Arrangement [illegible]
[illegible]

[illegible]

MIRONOV, Fedor Fedorovich; LAGUTINA, Ye.V., red.; BALDINA, N.F., tekhn. red.

[Physical culture in the control of tuberculosis]Fizicheskaia kul'tura v bor'be s tuberkulezom. Moskva, Medgiz, 1962. 37 p.

(TUBERCULOSIS) (EXERCISE THERAPY) (MIRA 15:11)

ROZANOVA, M. D., doktor med. nauk; AGRACHEV, G. I., kand. med. nauk;
VYSOKOVA, T. M., kand. med. nauk; KIDANOVA, Z. S.; MIRONOV, F. F.

Effect of exercise therapy on the functional state of adolescents with pulmonary tuberculosis. Probl. tub. 40 no.5:56-63 '62.
(MIRA 15:7)

1. Iz Moskovskogo nauchno-issledovatel'skogo instituta tuberkuleza Ministerstva zdravookhraneniya RSFSR (dir. - kandidat meditsinskikh nauk V. F. Chernyshev, zam. dir. po nauchnoy chasti - prof. D. D. Aseyev).

(TUBERCULOSIS) (EXERCISE THERAPY)

MIRONOV, F.M.

[illegible] new [illegible] manufacture of [illegible]
Koz.-obuv. prom. [illegible]

1. Glavnyy inzhener Ostashkovskogo kozhevennogo zavoda.

USSR Chemical Technology - Chemical Products and Their
Application - Leather. Fur. Gelatin. Tanning [illegible].
Technical Proteins.

Abs Jour : Referat Zhur - Khimiya, N [illegible]

Author : Lendenskiy, D.A., Mironov, F.[illegible], Lanenkin, M.[illegible]

Inst :

Title : Impregnation of Pigskin Footwear-Yuft with Acrylic Emulsion A.

Orig Pub : Legkaya prom-st', [illegible], N [illegible]

Abstract : To reduce water-permeability of yuft (to the norms specified in the GOST) it is impregnated with acrylic [illegible] emulsion A. Impregnating composition was applied to the flesh side 2-3 times, intermittently with pressing (after pre-drying) as well as without pressing. In all instances the water permeability per hour of pigskin yuft, following impregnation, was [illegible] m², [illegible] considerably below the norms of GOST. A procedure has been

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USSR/Chemical Technology - Chemical Products and Their Application - Leather. Fur. Gelatin. Tanning Agents. Technical Proteins. I-2

Abs Jour : Ref Zhur - Khimiya, No 9, 195[illegible], [illegible]

worked out for the impregnation of pigskin for wear-[illegible] with acidic acrylic emulsion A. The emulsion is brushed in 2-3 times with intermittent partial drying. Thereafter the leather is pressed on the flesh side, on a smooth surface press at 80-90° and pressure not exceeding 100 atmospheres. The thus treated leather does not differ in appearance from the unimpregnated leather.

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LENDENSKIY, D.A.; MIRONOV, F.V.; LAMENKIN, M.V.; AMBURG, S.L.

Impregnating Russian pig leather used in shoe manufacture with "A" brand acid acrylic emulsion. Obm.tekh.opyt. [MLP] no.27: 39-41 '56.

(Waterproofing) (Tanning) (MIRA 11:11)

MIRONOV, F.V., inzhener.

Possibilities in the use of SPS synthetic tannin. Leg.prom. 17 no.6:30-31 Je [illegible].
(Tanning materials (MIRA 10:8)

MIRONOV, F.V.

LASHENKIN, M.V.; KRYUCHKOV, A.I.; MIRONOV, F.V.

Manufacturing glove leather from kidskins and sheepskins. Leg. prom. 18 no.2:44-46 F '58. (MIRA 11:2)

(Tanning)

LANENKIN, M.V., inzh.; LENDENSKIY, D.A., inzh.; MIRONOV, F.V., inzh.

Animal fat substitutes. Leg. prom. 18 no.3:48-49 Mr '58. (MIRA 11:4)
(Oils and fats)

MIRONOV, F.V., inzh.; SHESTAKOVA, I.S., prof., doktor tekhn.nauk

New developments in the investigation of willow-bark extracts.
Kozh.-obuv.prom. 2 no.3:22-26 Mr '60. (MIRA 14:5)
(Tanning materials)

MIRONOV, F.V., inzh.; SHESTAKOVA, I.S., prof.

Effect of the quality of willow bark tanning extracts on the properties of Russian leather. Kozh.-obuv.prom. 2 no.6:13-18 Je '60.

(Tanning) (MIRA 13:9)

MIRONOV, F.

Improving the quality of leather. Kozh.-obuv.prom. 2 no.9:37 S '60. (MIRA 13:10)

(Leather)

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240

FEDOTOV, F.I.; MIRONOV, F.V.

Refining the Russian cowhide leather. Kozh.-obuv.prom. 3 no.2:25 F '61. (MIRA 14:4)

(Leather)

MIRONOV, F.V.

From work practices of the Ostashkov Leather Factory. Kozh.-obuv. prom. 3 no.4:28-30 Ap '61. (MIRA 14:5)
(Ostashkov--Leather industry)
(Tanning)

ZURABYAN, K.M.; MIRONOV, F.V.; MORGULIS, I.A.

New method of regulating the penetration depth of dye coatings in the refining of leather. Kozh.-obuv.prom. 3 no.1:25-[illegible] (MIRA 15:1)

(Dyes and dyeing—Leather)

MIRONOV, F.Ya.; KOZHEVNIKOVA, Ye.N.

Diagnostic significance of calcium in blood serum in various forms of acute pancreatitis. Khirurgiia 32 no.11:36-39 N '56 (MIRA 10:3)

1. Iz 1-y khirurgicheskoy kliniki (zav. - prof. S.V.Lobachev) i TSentral'noy laboratorii (zav. - dotsent V.V.Novosel'skaya) Instituta imeni Sklifosovskogo (glavnyy khirurg - prof. B.A.Petrov, dir. - zasluzhennyy vrach USSR M.M.Tarasov)
(PANCREATITIS, diag.
calcium determ. in blood serum)
(CALCIUM, in blood
determ. in diag. of acute pancreatitis)

MIRONOV, G.A.

Geology of the contact zone between the Chinorsayskaya intrusion and the Govazmon tungsten deposits (Zeravshan Range). Izv. Otd. est. nauk AN Tadzh. SSR no.1:9-21 '58. (MIRA 12:1)

1. Institut geologii AN Tadzhikskoy SSR.
(Zeravshan Range--Geology, Structural)
(Zeravshan Range--Tungsten)

PHASE I BOOK EXPLOITATION SOV/6529

Krinitskiy, N. A., G. A. Mironov, and G. D. Frolov

Programmirovaniye (Programming). Moscow, Fizmatgiz, 1963. 383 p. (Series: Spravochnaya matematicheskaya biblioteka) Errata slip inserted. 40,000 copies printed.

Ed. (Title page): M. R. Shura-Bura; Eds. of the series: L. A. Lyusternik and A. R. Yanpol'skiy; Ed.: Yu. M. Bezborodov; Tech. Ed.: N. Ya. Murashova.

PURPOSE: This handbook is intended for students in schools of higher education and universities, and for engineers and scientific workers who either use or service electronic computers.

COVERAGE: The book deals with problems of programming. Theoretical elements of program-controlled computers are briefly discussed and classified, and the basic operations of computers are described. Special computer characteristics, the sequence of problem solving, and operational programming methods are given. The application of

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certain conventional methods to programming is described. The method of standard subroutines is presented in its two variants (compilation and interpretation systems). Basic information is given on the automation of programming by means of an operator-programmer. In addition, the book includes short descriptions of the principal Soviet electronic digital computers (the Ural-1, Ural-2, "Setun'," M-2, M-3, BESM-2, and "Strela"). The first part of the book (chapters 1—7) was written by N. A. Krinitskiy, and the second part (chapters 8—14), by G. A. Mironov and G. D. Frolov. The authors thank L. A. Lyusternik, A. A. Lyapunov, M. R. Shura-Bura and A. R. Yanpol'skiy for their assistance. There are 60 references, all Soviet.

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